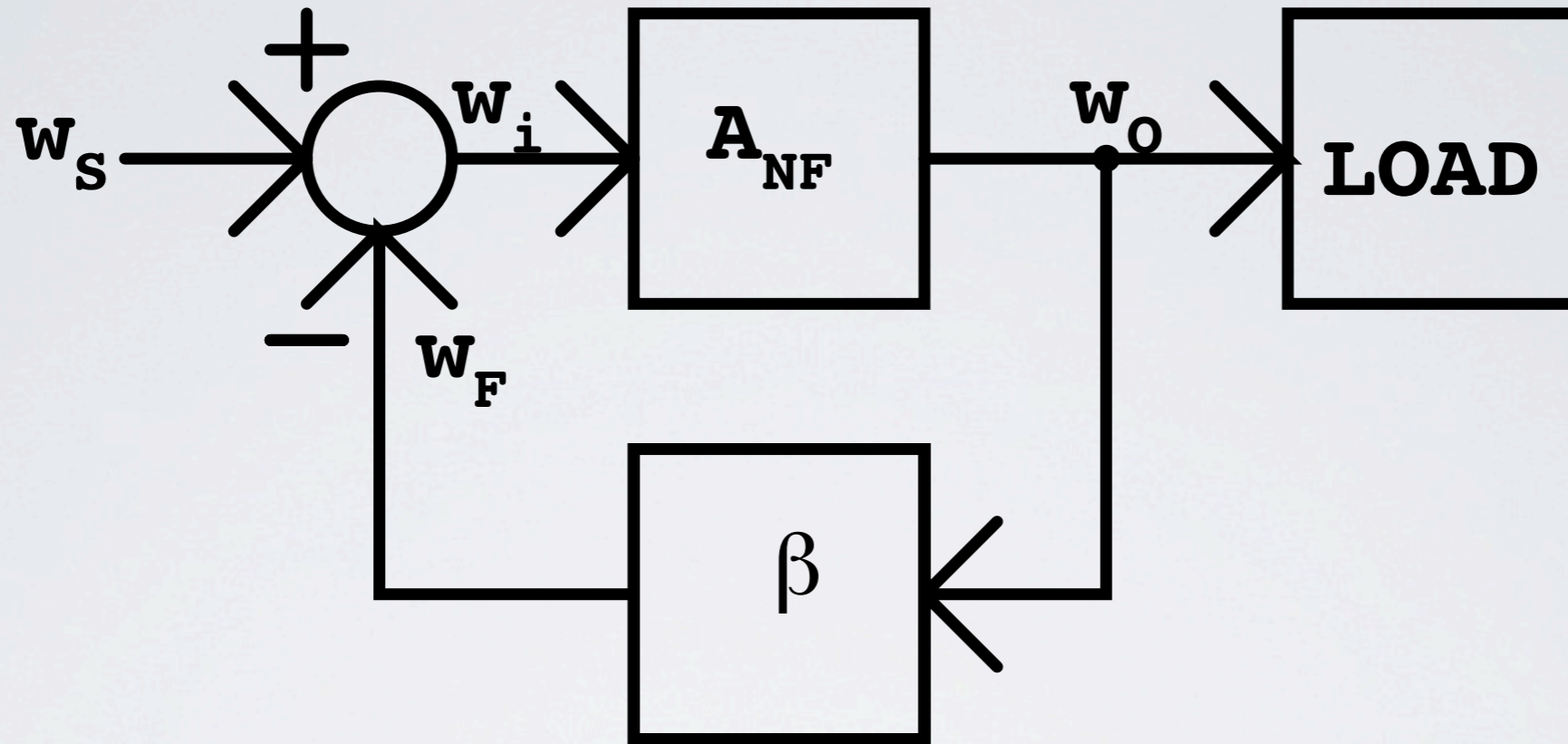


RETRO-ALIMENTACIÓN

Conceptos Básicos
INEL 5207 - Enero 2013

Sistema General



$$w_o = A_{NF}w_i = A_{NF}(w_S - \beta w_o)$$

$$w_o = \frac{A_{NF}}{1 + \beta A_{NF}}w_S = A_F w_S = \frac{A_{NF}}{D}$$

$$\begin{aligned}
A_f &= \frac{A}{1 + \beta A} \\
&= \frac{A}{T} \frac{1}{1 + \frac{1}{T}} \\
&= A_{ideal} \frac{1}{1 + \frac{1}{T}} \\
A_{ideal} &= \lim_{\beta A \rightarrow \infty} A_f = \frac{A}{T} = \frac{1}{\beta} \\
A_f &= \frac{1}{\beta} \frac{1}{1 + \frac{1}{T}}
\end{aligned}$$

La cantidad

$$\frac{1}{1 + \frac{1}{T}}$$

expresa cuanto se aparta la ganancia de nuestro amplificador del caso ideal. Por esto es a veces denominada la *función de error*.

VENTAJAS

- Reduce la sensibilidad a parámetros
- Aumenta el ancho de banda
- Reduce la distorsión
- Mejora la resistencia de entrada y salida
- Desventaja: reduce la ganancia.

SENSITIVIDAD

$$\begin{aligned} S_P^{A_F} &= \frac{P}{A_F} \frac{dA_F}{dP} = \frac{P}{A_F} \frac{d \frac{A_{NF}}{1 + \beta A_{NF}}}{dP} \\ &= \frac{P}{A_F} \frac{d}{dA_{NF}} \frac{A_{NF}}{1 + \beta A_{NF}} \frac{dA_{NF}}{dp} \\ &= \frac{P}{A_F} \frac{dA_{NF}}{dp} \left(\frac{1}{1 + \beta A_{NF}} - \frac{\beta A_{NF}}{(1 + \beta A_{NF})^2} \right) \\ &= \frac{P}{A_{NF}} \frac{dA_{NF}}{dp} \left(1 - \frac{\beta A_{NF}}{1 + \beta A_{NF}} \right) \\ &= \frac{P}{A_{NF}} \frac{dA_{NF}}{dp} \frac{1}{1 + \beta A_{NF}} \\ &= S_P^{A_{NF}} \frac{1}{1 + \beta A_{NF}} \end{aligned}$$

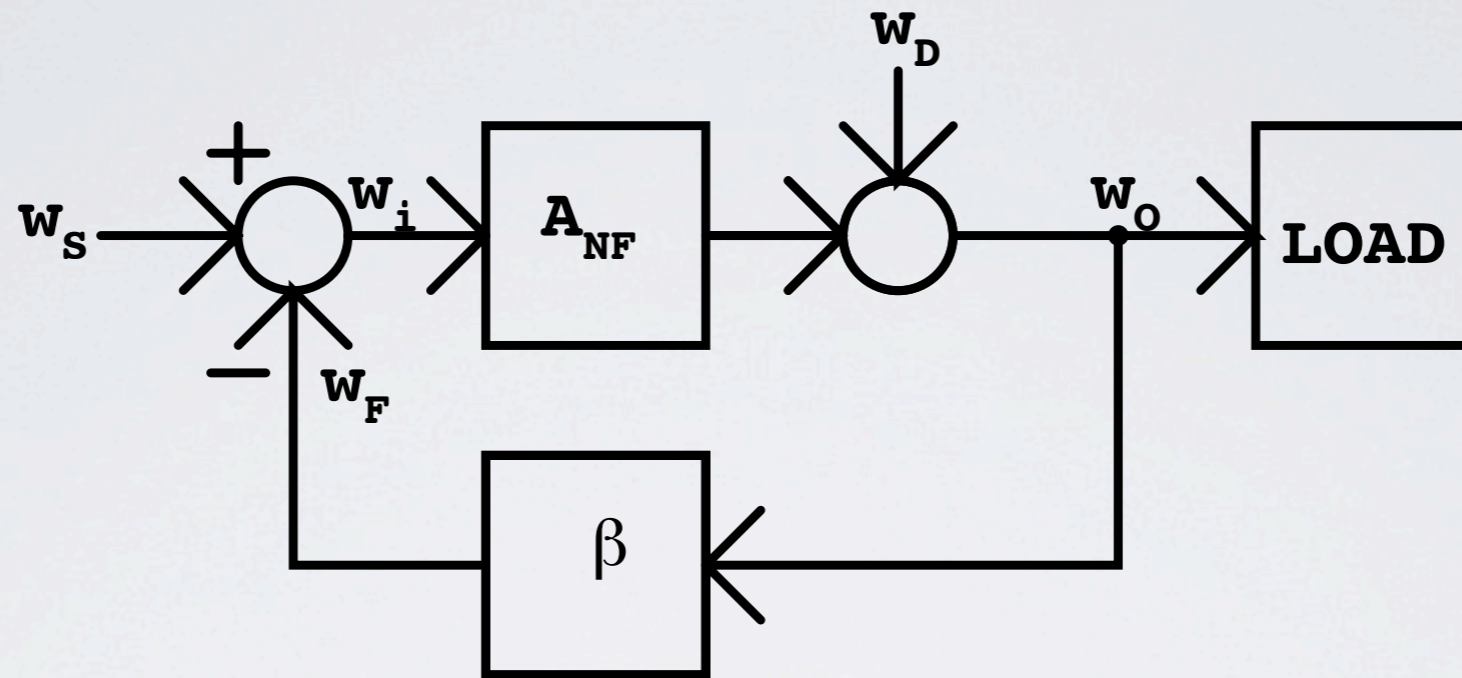
RESPUESTA DE BAJA FREC.

$$\begin{aligned}A_{NF}(s) &= A_{mid} \frac{s}{s + \omega_L} \\A_F(s) &= \frac{A_{mid} \frac{s}{s + \omega_L}}{1 + \beta A_{mid} \frac{s}{s + \omega_L}} \\&= \frac{A_{mid} s}{s + \omega_L + \beta A_{mid} s} \\&= \frac{A_{mid} s}{s(1 + \beta A_{mid}) + \omega_L +} \\&= \frac{A_{mid}}{1 + \beta A_{mid}} \frac{s}{s + \frac{\omega_L}{1 + \beta A_{mid}}}\end{aligned}$$

RESPUESTA DE ALTA FREC.

$$\begin{aligned} A_{NF} &= A_{mid} \frac{\omega_H}{s + \omega_H} \\ A_F(s) &= \frac{A_{mid} \frac{\omega_H}{s + \omega_H}}{1 + \beta A_{mid} \frac{\omega_H}{s + \omega_H}} \\ &= \frac{A_{mid} \omega_H}{s + \omega_H + \beta A_{mid} \omega_H} \\ &= \frac{A_{mid} \omega_H}{s + \omega_H (1 + \beta A_{mid})} \\ &= \frac{A_{mid}}{1 + \beta A_{mid}} \frac{\omega_H (1 + \beta A_{mid})}{s + \omega_H (1 + \beta A_{mid})} \end{aligned}$$

DISTORCIÓN

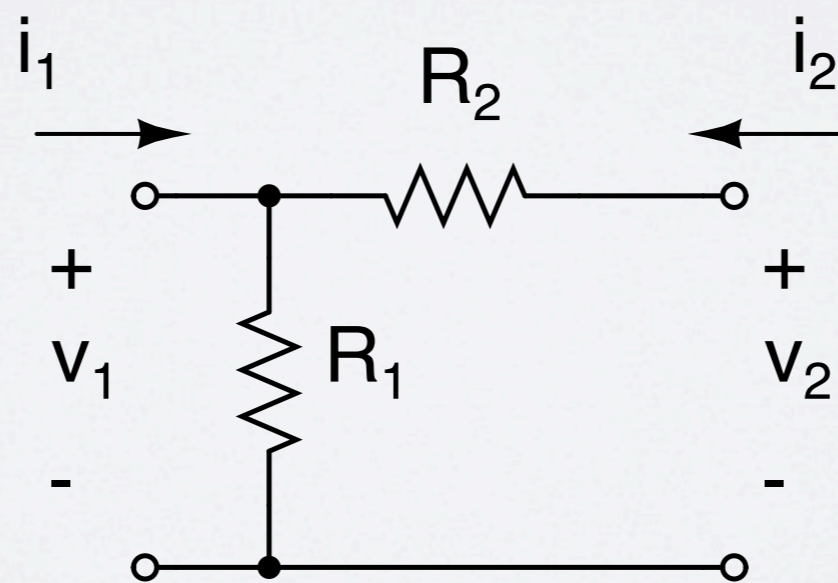
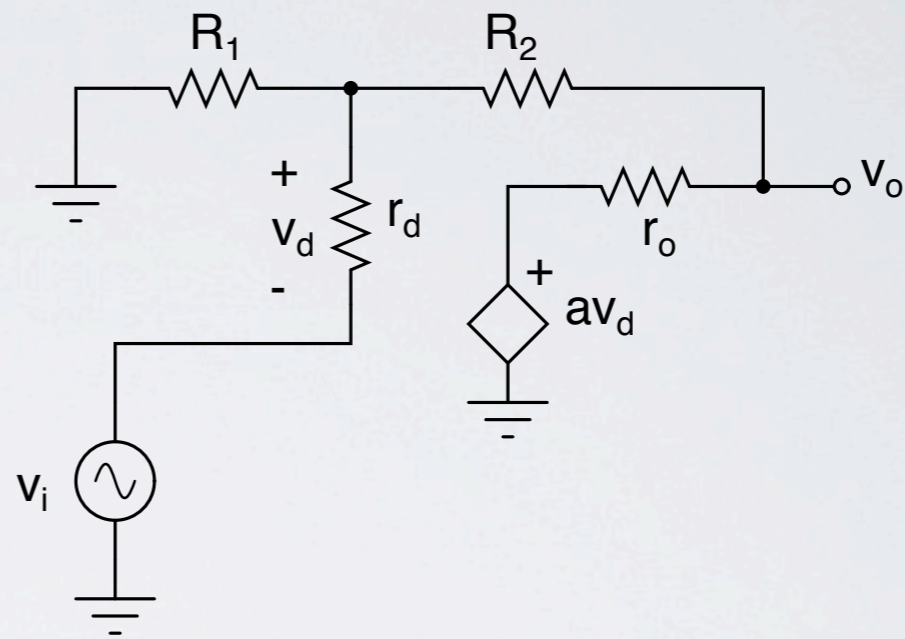
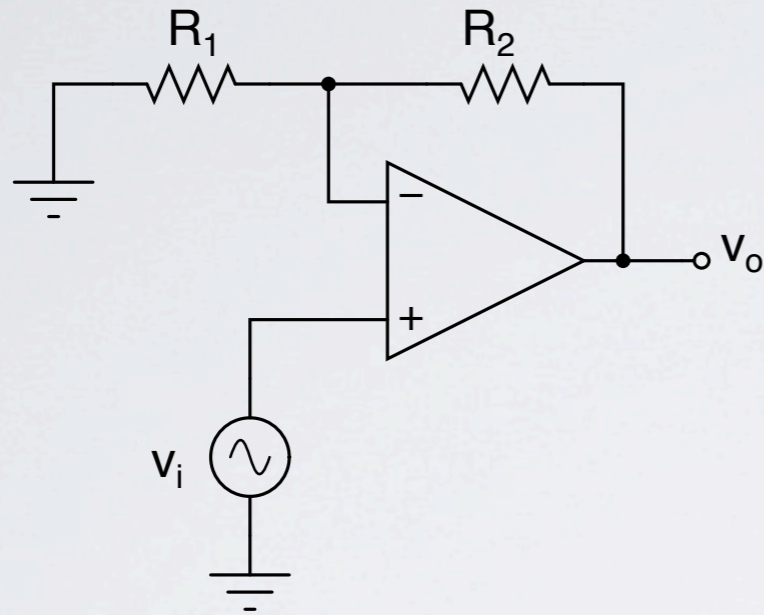


$$\begin{aligned}w_o &= w_D + A_{NF}w_i \\ &= w_D + A_{NF}(w_S - \beta w_o) \\ &= \frac{w_D}{1 + \beta A_{NF}} + \frac{A_{NF}}{1 + \beta A_{NF}}\end{aligned}$$

1.5 Negative feedback

- 1.45** A voltage amplifier has $a = 10^5$ V/V and $v_i = 10$ mV. Find v_d , v_f , v_o , A , T , and the percentage deviation of A from A_{ideal} for $\beta = 10^{-3}$ V/V, 10^{-2} V/V, 10^{-1} V/V, and 1 V/V. Compare the various cases and comment.
- 1.46** (a) Find the desensitivity factor of a negative-feedback system with $a = 10^3$ and $A = 10^2$. (b) Find A exactly via Eq. (1.40), and approximately via Eq. (1.49) if a drops by 10%. (c) Repeat (b) for a 50% drop in a ; compare with (b) and comment.
- 1.47** You are asked to design an amplifier with a gain A of 10^2 V/V that is accurate to within $\pm 0.1\%$, or $A = 10^2$ V/V $\pm 0.1\%$. All you have available are amplifier stages with $a = 10^4$ V/V $\pm 25\%$ each. Your amplifier can be implemented using a cascade of basic stages, each employing a suitable amount of negative feedback. What is the minimum number of stages required? What is the β of each stage?

AMP. SIN INVERSIÓN



$$\beta = \frac{v_1}{v_2} \Big|_{i_1=0} = \frac{R_1}{R_1 + R_2}$$

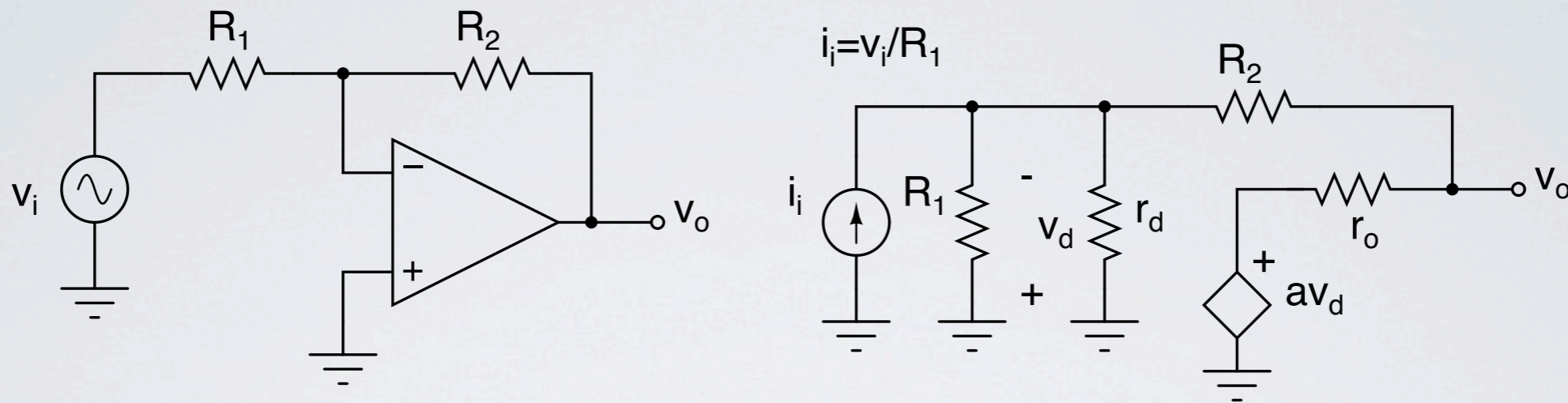
$$T = \frac{v_o}{v_i} = \frac{R_{22}}{r_o + R_{22}} a \frac{r_d}{r_d + R_{11}} \frac{R_1}{R_1 + R_2}$$

Para un diseño correcto, $r_d \gg R_{11}$ y $r_o \ll R_1 + R_2$, y.

$$T \approx \frac{aR_1}{R_1 + R_2} = a\beta$$

$$A_f = \frac{1}{\beta} \frac{1}{1 + \frac{1}{T}} = \left(1 + \frac{R_2}{R_1} \right) \frac{1}{1 + \frac{1}{T}}$$

AMP CON INVERSIÓN



$$T = a \frac{R_1 \parallel R_2 \parallel r_d}{r_o + R_2}$$

Usualmente, $r_d \gg (R_1 \parallel R_2)$ y $r_o \ll R_2$, así que

$$T \approx a \frac{R_1}{R_1 + R_2}$$

Esta es la misma expresión que obtuvimos para el amplificador sin inversión.

$$A_{vf} = \frac{v_o}{v_i} = -\frac{R_2}{R_1} \frac{1}{1 + \frac{1}{T}}$$

1.54 (a) Find A_{ideal} in the circuit of Fig. P1.54 if all resistances are equal. (b) Assuming $r_d \cong \infty$ and $r_o \cong 0$, find a_{min} such that the deviation of A from A_{ideal} is less than 0.1%.

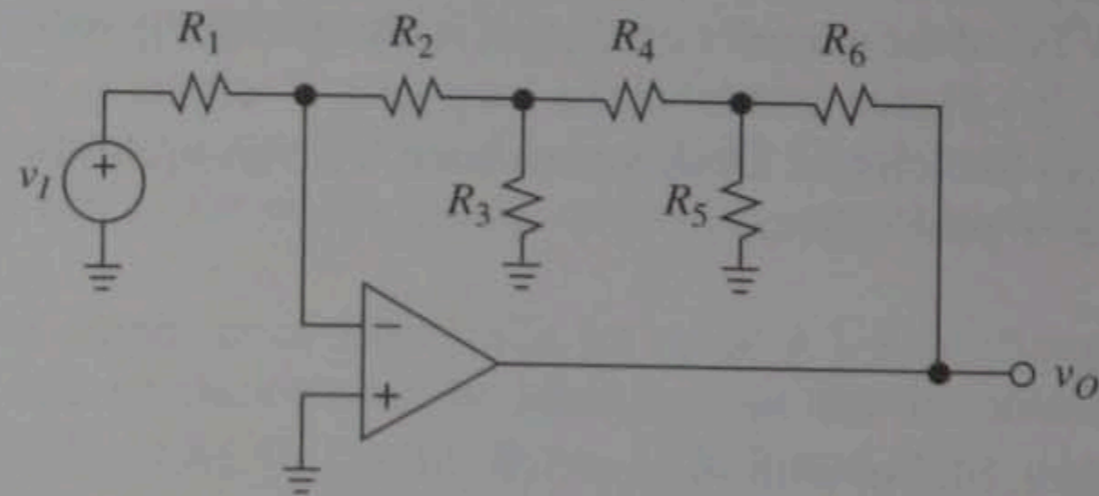


FIGURE P1.54