

CE/CS Amplifier Response at High Frequencies

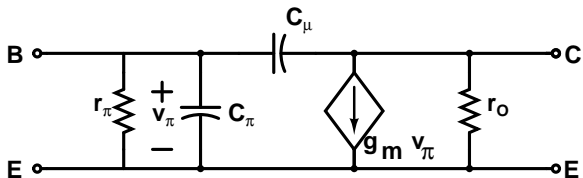
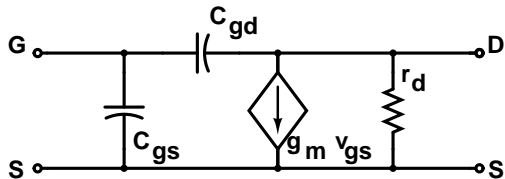
INEL 4202 - Manuel Toledo

August 20, 2012

Outline

- 1 High Frequency Models
- 2 Simplified Method
- 3 Common-emitter
- 4 Miller Theorem
- 5 Unity Gain Frequency

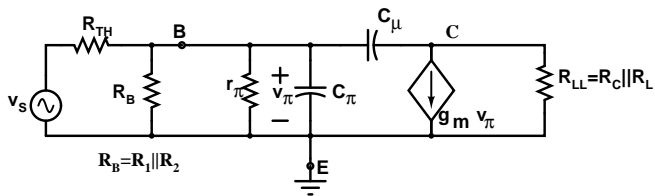
High Frequency Models



small-signal incremental model

PARASITIC CAPS LIMIT GAIN AT HIGH FREQS.

CE High Frequency Model



Open-circuit time constant method

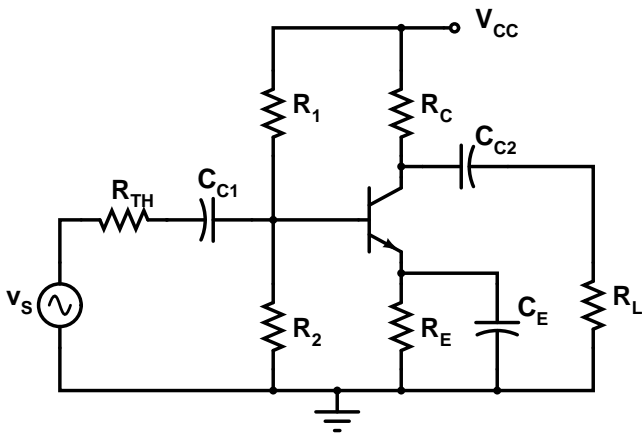
- 1 Replace all coupling and bypass caps by shorts
- 2 Select one parasitic cap; call it C_{H1}
- 3 Replace all other parasitic caps by open circuits
- 4 Find resistance seen by C_{H1} ; call it R_{H1}
- 5 High frequency pole associated with C_{H1} is

$$\omega_{H1} = \frac{1}{C_{H1}R_{H1}}$$

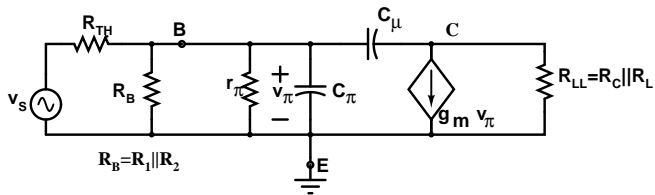
- 6 Repeat above steps for each parasitic cap
- 7 Find equivalent high frequency cutoff

$$\omega_H = \frac{1}{\sum_{i=1}^n \frac{1}{\omega_{Hi}}}$$

Single-stage amplifier



Single-stage amplifier

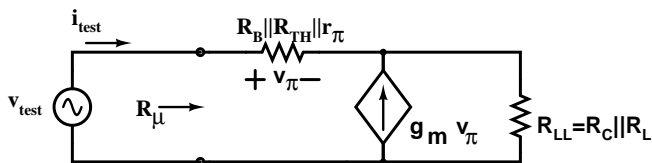


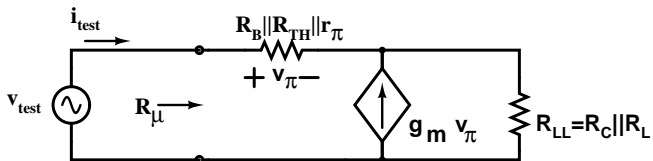
Resistance

Seen by C_π :

$$R_\pi = r_\pi \parallel R_B \parallel R_{TH}$$

Seen by C_μ :



R_{μ} Resistance seen by C_{μ} 

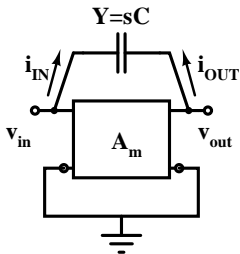
$$v_{\pi} = i_{test}(R_B || R_{TH} || r_{\pi})$$

R_{μ}

Applying KVL on the external loop yields

$$\begin{aligned}
 v_{test} &= v_{\pi} + (i_{test} + g_m v_{\pi}) R_{LL} \\
 &= i_{test} (R_B \parallel R_{TH} \parallel r_{\pi}) \\
 &\quad + (1 + g_m (R_B \parallel R_{TH} \parallel r_{\pi})) i_{test} R_{LL} \\
 R_{\mu} &= \frac{v_{test}}{i_{test}} \\
 &= R_B \parallel R_{TH} \parallel r_{\pi} + R_{LL} \\
 &\quad + g_m (R_B \parallel R_{TH} \parallel r_{\pi}) R_{LL}
 \end{aligned}$$

Miller Theorem



Assume that $A_m = \frac{v_{OUT}}{v_{IN}}$ is negative and is independent of $Y = sC$.

Use

$$v_{OUT} = A_m v_{IN}$$

$$v_{IN} = v_{OUT} / A_m$$

Miller Theorem

Input:

$$\begin{aligned}i_{IN} &= Y(v_{IN} - v_{OUT}) \\ &= sC(1 - A_m)v_{IN} = sC_{IN}v_{IN}\end{aligned}$$

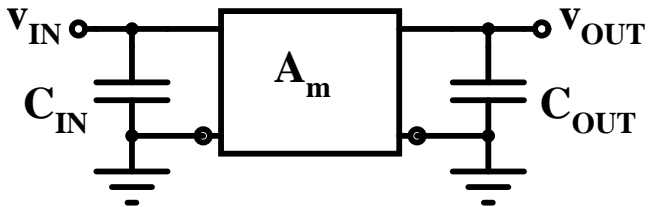
i.e. from the input C looks like a bigger capacitor $C(1 - A_m)$.

Output:

$$\begin{aligned}i_{OUT} &= Y(v_{OUT} - v_{IN}) \\ &= sC\left(1 - \frac{1}{A_m}\right)v_{OUT} = sC_{OUT}v_{OUT}\end{aligned}$$

i.e. from the output C looks like a capacitor $C\left(1 - \frac{1}{A_m}\right) \approx C$.

Miller Theorem



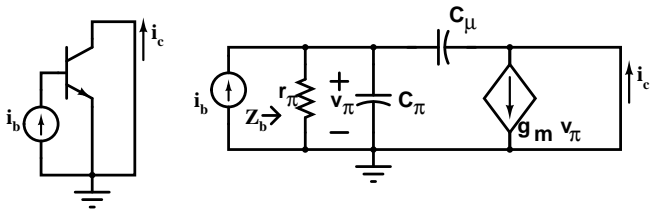
Miller Theorem

To apply Miller's Theorem, make sure that

- A_m is negative
- A_m is real, i.e. load is resistive

Unity-gain frequency: f_t

f_t : frequency at which the transistor's $\beta = 1$.



Unity-gain frequency: f_t

$$i_c = g_m v_\pi - v_\pi s C_\mu$$

$$v_\pi = i_b \times Z_b$$

$$\begin{aligned} Z_b &= r_\pi \parallel \frac{1}{sC_\pi} \parallel \frac{1}{sC_\mu} \\ &= \frac{1}{\frac{1}{r_\pi} + sC_\pi + sC_\mu} \\ &= \frac{r_\pi}{1 + sr_\pi(C_\pi + C_\mu)} \end{aligned}$$

Unity-gain frequency: f_t

$$\begin{aligned}\beta(s) &= \frac{i_c}{i_b} \\ &= \frac{g_m r_\pi - s r_\pi C_\mu}{1 + s r_\pi (C_\pi + C_\mu)} \\ &\approx \frac{\beta_0}{1 + s r_\pi (C_\pi + C_\mu)}\end{aligned}$$

Midband $\beta \equiv \beta_0 = g_m r_\pi$

β has a pole at

$$\omega_\beta = \frac{1}{r_\pi (C_\pi + C_\mu)}$$

Unity-gain frequency: f_t

f_t : f at which $|\beta(s)| = 1$

$$\beta_0^2 = 1 + \frac{\omega_t^2}{\omega_\beta^2}$$

$$\omega_t = \omega_\beta \sqrt{\beta_0^2 - 1} \approx \beta_0 \omega_\beta$$

Data sheet often specifies f_t and C_μ ; C_π can then be found from above equations.

Example

A common-source amplifier is constructed with a $10\mu F$ bypass capacitor in parallel with a $1k\Omega$ resistor, both connected to the FET's source terminal. The equivalent resistance "seen" by the bypass capacitor is 100Ω . At high frequencies there is a single pole located at $1MHz$. If the amplifier's midband gain is $80dB$, find an expression for the amplifier's gain as a function of the complex frequency s , valid for low-, mid- and high-frequencies.

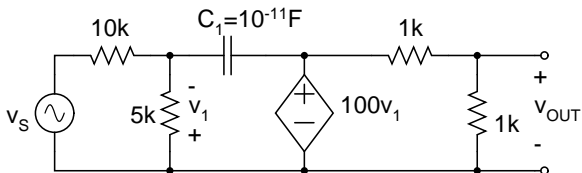
A common-source amplifier is constructed with a $10\mu F$ bypass capacitor in parallel with a $1k\Omega$ resistor, both connected to the FET's source terminal. The equivalent resistance "seen" by the bypass capacitor is 100Ω . At high frequencies there is a single pole located at $1MHz$. If the amplifier's midband gain is $80dB$, find an expression for the amplifier's gain as a function of the complex frequency s , valid for low-, mid- and high-frequencies.

ANSWER:

$$A_v(s) = -10^4 \frac{s + 10^2}{s + 10^3} \frac{1}{s/2\pi \times 10^6 + 1}$$

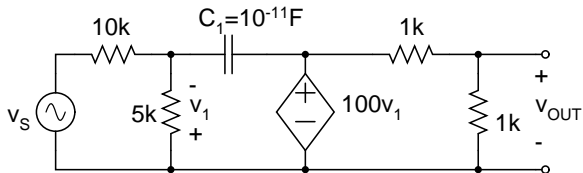
Example

For the circuit shown below, find (i) the pole frequency applying Miller's theorem; (ii) the pole frequency using the open-circuit time constant method; and (iii) an expression for the voltage gain $A_V(s) = \frac{V_{OUT}}{V_S}$ as a function of complex frequency s , valid for mid- and high-frequencies.



Example

For the circuit shown below, find (i) the pole frequency applying Miller's theorem; (ii) the pole frequency using the open-circuit time constant method; and (iii) an expression for the voltage gain $A_V(s) = \frac{V_{OUT}}{V_S}$ as a function of complex frequency s , valid for mid- and high-frequencies.



ANSWER: (i) 297krps ; (ii) 297krps (iii) $A_V(s) = -16.7 \frac{1}{s/297\text{krps} + 1}$

Prob. 6.110

A CS amplifier is specified to have $g_m = 5\text{mA/V}$, $r_o = 40\text{k}\Omega$, $C_{gs} = 2\text{pF}$, $C_{gd} = 0.1\text{pF}$, $C_L = 1\text{pF}$, $R_{sig} = 20\text{k}\Omega$, and $R_L = 40\text{k}\Omega$. (a) Find the low-frequency gain A_M and use open-circuit time constants to estimate the 3-dB frequency f_H . Hence determine the gain-bandwidth product. (b) If a 500Ω resistance is connected in the source lead, find the new values of $|A_M|$, f_H , and the gain-bandwidth product. Assume $g_{mb} = 1\text{mA/V}$.

Prob. 6.110

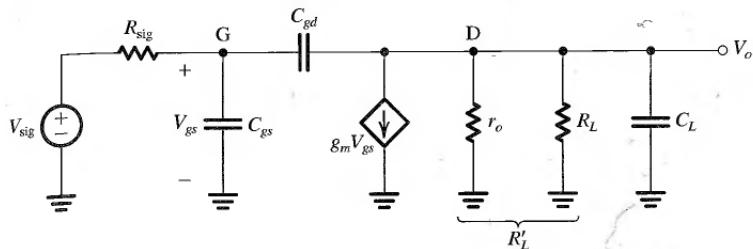


FIGURE 6.20 High-frequency equivalent-circuit model of the common-source amplifier. For the common-emitter amplifier, the values of V_{sig} and R_{sig} are modified to include the effects of r_{π} and r_s ; C_{gs} is replaced by C_{π} , V_{gs} by V_{π} , and C_{gd} by C_{μ} .