

NAME:

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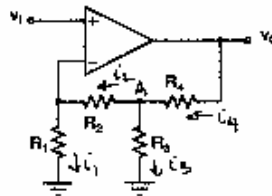
STUDENT NO.:

Ex 2b

University of Puerto Rico  
 Electrical and Computer Engineering Department  
 INEL 4202 - Electronics II - Fall 2002 - Exam 2b - Prof. M. Toledo  
 THERE ARE THREE PROBLEMS - BE CLEAR ON LOOSE POINTS

1. For the amplifier shown below, assume an ideal opamp.

- (a) Derive an expression for  $A_v = v_o/v_i$  in terms of  $R_1, R_2, R_3$  and  $R_4$ ; (25 points)  
 (b) Find  $A_v = v_o/v_i$  if  $R_1 = R_3 = 1\text{k}\Omega$ ,  $R_2 = 10\text{k}\Omega$  and  $R_4 = 20\text{k}\Omega$ ; (5 points)



$$(a) \quad v_- = v_+ = v_i \quad ; \quad i_1 = v_i/R_1 = i_2 \quad ; \quad v_A = v_- + i_2 R_2$$

$$v_A = v_i + \frac{R_2}{R_1} v_i = v_i \left(1 + \frac{R_2}{R_1}\right)$$

$$i_3 = \frac{v_A}{R_3} = \frac{v_i}{R_3} \left(1 + \frac{R_2}{R_1}\right)$$

$$v_o = i_4 R_4 + v_A = i_3 R_4 + i_2 R_4 + v_A$$

$$= v_i \frac{R_4}{R_3} \left(1 + \frac{R_2}{R_1}\right) + \frac{R_4}{R_1} v_i + v_i \left(1 + \frac{R_2}{R_1}\right)$$

$$\boxed{\frac{v_o}{v_i} = \frac{R_4}{R_1} + \left(1 + \frac{R_4}{R_3}\right) \left(1 + \frac{R_2}{R_1}\right)}$$

$$(b) \quad \frac{v_o}{v_i} = \frac{20\text{k}}{1\text{k}} + \left(1 + \frac{20\text{k}}{1\text{k}}\right) \left(1 + \frac{10\text{k}}{1\text{k}}\right)$$

$$= 20 + 21 \times 11 = \boxed{+251}$$

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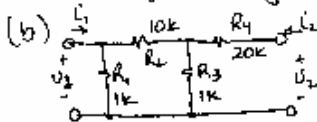
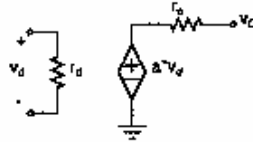
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2. For the amplifier shown in problem 1, assume that the opamp can be represented with the model shown below, with  $r_d = 10k\Omega$ ,  $a = 10^4 V/V$  and  $r_o = 100\Omega$ .

- Identify the type of feedback being used. (10 points)
- Draw a diagram of the feedback network. (10 points)
- Find the feedback network's  $R_{11}$ ,  $R_{22}$  and  $\beta$  as defined in lecture. (10 points)
- Draw a diagram of the non-feedback amplifier that must be analyzed to properly use the feedback method discussed in lecture. (10 points)
- Find the non-feedback amplifier gain that must be used in the feedback method discussed in lecture. (10 points)

(a) voltage-sampling,  
voltage-mixing

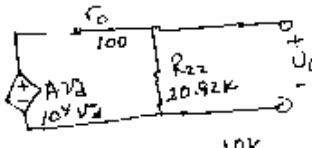


(c)  $R_{11} = \frac{v_1}{i_1} \Big|_{v_2=0} = [(20k // 1k) + 10k] // 1k = 916\Omega$

$R_{22} = \frac{v_2}{i_2} \Big|_{v_1=0} = 11k // 1k + 20k = 20.92k\Omega$

$\beta = \frac{v_1}{v_2} \Big|_{v_1=0} = \frac{1}{R_{22}} \frac{1k}{12k} (1k) = \frac{1}{251} = .0394$

(d)



$\frac{v_o}{v_i} = \frac{20.92k}{21.02k} (10^4) \frac{10k}{10,916\Omega} = 9117 V/V$

3. An amplifier will be used in a feedback configuration. Its d.c. gain  $A_0 = 10^4$ . Its frequency response displays poles at  $f_{p1} = 20\text{kHz}$ ,  $f_{p2} = 500\text{kHz}$ ,  $f_{p3} = 20\text{MHz}$ . You want to use this amplifier to obtain a gain with feedback  $A_f \approx \frac{1}{\beta} = 100$ . Determine the new position of  $f_{p1}$  if the pole-shifting technique will be used to compensate the amplifier for a phase margin of  $45^\circ$ . (20 points)

$$\begin{aligned} A(f_{p2}) &\approx 80\text{dB} - (20\text{dB/dec}) \left( \log \frac{f_{p2}}{f_{p1}} \text{ decs} \right) \\ &= 80\text{dB} - 20\text{dB/dec} \times 1.4 \text{ dec.} \\ &= \text{52dB} \end{aligned}$$

(For a more accurate estimate of  $A(f_{p2})$  subtract an additional  $3\text{dB}$  to correct the asymptotic behavior being used; or use the gain formula  $A(f) = \frac{A_0}{\prod \sqrt{1+(f/f_p)^2}}$ )

Since  $(1/\beta)_{\text{dB}} = 40\text{dB}$ , for  $\phi_m = 45^\circ$   $A(f_{p2})$  must drop by  $12\text{dB}$ .  $\therefore$  move the first pole down by  $12\text{dB}/20\text{dB/dec} = 0.6 \text{ decs.}$

or  $0.6 = \log(f_{p1}/f_{\text{new}})$

yields

$$f_{\text{new}} \approx 5\text{kHz}$$

as the new frequency of the 1<sup>st</sup> pole.