

1. An amplifier was designed using a bipolar transistor with $C_{\mu} = C_{\pi} = 5\text{pF}$, a $10\mu\text{F}$ coupling capacitors C_C and a $50\mu\text{F}$ bypass capacitor C_B . The resistances seen by these capacitors are $R_{\mu} = 10\text{k}\Omega$, $R_{\pi} = 1\text{k}\Omega$, $R_C = 1\text{k}\Omega$, $R_B = 100\Omega$, respectively. A $1\text{k}\Omega$ resistor is connected in parallel with C_B and the amplifier's midband gain is 1234.

(a) Find the approximate low and high effective cut-off frequencies. (10 points)

(b) Write an expression for the gain as a function of frequency, valid for all frequency bands. (10 pts)

$$\begin{aligned} \omega_{\mu} &= \frac{1}{5\text{pF} \times 10\text{k}\Omega} = 2 \times 10^7 \text{ rps} \\ \omega_{\pi} &= \frac{1}{5\text{pF} \times 1\text{k}\Omega} = 2 \times 10^8 \text{ rps} \end{aligned} \left. \vphantom{\begin{aligned} \omega_{\mu} \\ \omega_{\pi} \end{aligned}} \right\} \text{high freq poles}$$

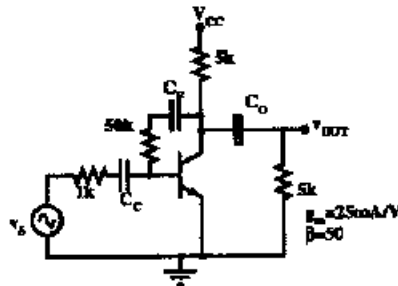
$$\begin{aligned} \omega_C &= \frac{1}{10\mu\text{F} \times 1\text{k}\Omega} = 100 \text{ rps} \\ \omega_B &= \frac{1}{50\mu\text{F} \times 100\Omega} = 200 \text{ rps} \end{aligned} \left. \vphantom{\begin{aligned} \omega_C \\ \omega_B \end{aligned}} \right\} \text{low freq. poles}$$

$$\omega_{ZB} = \text{zero due to bypass cap.} = \frac{1}{50\mu\text{F} \times 1\text{k}\Omega} = 20 \text{ rps}$$

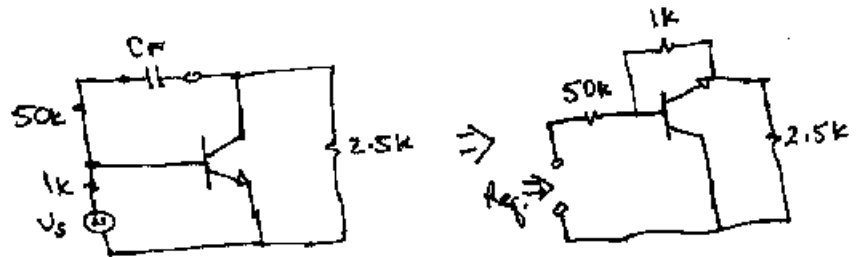
$$(b) A_v = 1234 \frac{s+20}{s+200} \frac{s}{s+100} \frac{2 \times 10^7}{s+2 \times 10^7} \frac{2 \times 10^8}{s+2 \times 10^8}$$

where $s = j\omega$

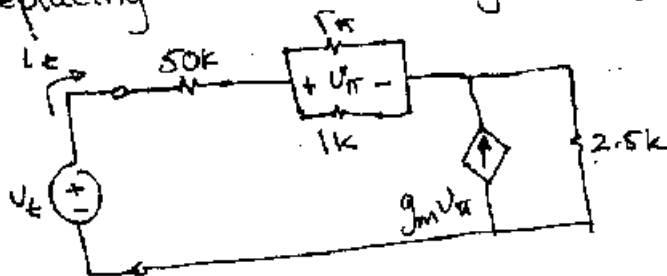
2. Use the *short-circuit time-constant* method to determine the resistance seen by C_F in the following amplifier. You should use the low-frequency transistor model. (20 pts)



a.c. circuit :



Replacing the transistor by its equivalent circuit, we get



$$r_{\pi} = \frac{\beta}{g_m} = \frac{50}{25 \text{ mA/V}} = 2 \text{ k}\Omega$$

$$v_{\pi} = (1 \text{ k} \parallel 2 \text{ k}) i_t = 666.7 i_t$$

KVL on outer loop:

$$v_t = 50 \text{ k} i_t + 666.7 i_t + 2.5 \text{ k} (i_t + g_m v_{\pi})$$

$$v_t = 53167 \Omega \times i_t + 2.5 \text{ k} \times 25 \text{ mA/V} \times 666.7$$

$$v_t = 94.8 \text{ k}\Omega \times i_t$$

$$R_{EQ} = 94.8 \text{ k}\Omega$$

3. A power amplifier capable of providing up to 25 watts to a 50 Ohms load is needed. To reduce distortion, the amplifier's output voltage should never exceed 80% of the power supply voltage.

(a) Design a Class-A amplifier to satisfy these requirements. You should determine (i) the power supply voltages, average current, maximum instantaneous current, and power; (ii) the transistor's required power rating, average collector current, maximum instantaneous collector current, and maximum collector-to-emitter voltage; (iii) the current source's current. (10 points)

(b) Design a Class-B amplifier to satisfy these requirements. You should determine (i) the power supply voltages, average current, maximum instantaneous current, and power; (ii) the transistor's required power rating, average collector current, maximum instantaneous collector current, and maximum collector-to-emitter voltage. (10 points)

(c) Determine the efficiency of the amplifiers designed in parts (a) and (b) when the output voltage is half of the maximum specified. (5 points)

(a) $P_{Lmax} = 25W$; $R_L = 50\Omega \Rightarrow V_{opeak} = \sqrt{2 P_{Lmax} R_L} = \sqrt{2(25W)(50\Omega)} = 50V$

Since $V_{opeak} \leq .8V_{CC}$ it follows that $V_{CC} = 62.5V$

The current-source should be selected $I_{EE} = \frac{62.5V}{50\Omega} = 1.25A$

i. $I_{AVE} = I_{EE} = 1.25A$

max. current occurs when $V_o = V_{opeak} = 50V$; $i_{Lpeak} = 1A$

$I_{psmax} = 1A + 1.25A = i_{Lpeak} + I_{EE} = 2.25A = I_{psmax}$

$P_{PS} = I_{EE} \times 2V_{CC} = 2(62.5V)(1.25A) = 156.25W = P_{PS}$

ii. transistor requirements

$P_D = \frac{1}{2} P_{PS}$

$P_D = 78.125W$

$i_{CAVE} = I_{EE} = 1.25A$

$i_{Cmax} = I_{psmax} = 2.25A$

$V_{CEmax} =$

$V_{CC} + V_{opeak} = 62.5V + 50V = 112.5V$

iii. $I_{EE} = 1.25A$

ii) Class B

i.

$$V_{CC} = 62.5 \text{ V} \quad (\text{see part a})$$

$$i_{PS_{\text{ave}}} = \frac{I_{L_{\text{peak}}}}{\pi} = \frac{50 \text{ V} / 50 \Omega}{\pi} = \boxed{i_{PS_{\text{ave}}} = 0.318 \text{ A}}$$

$$\boxed{i_{PS_{\text{max}}} = I_{L_{\text{peak}}} = 1 \text{ A}}$$

$$P_{PS} = 0 \text{ W for } 0 \text{ V output}$$

$$= i_{PS_{\text{ave}}} \times V_{CC} \times 2 = 2(62.5 \text{ V})(0.318 \text{ A}) \approx 40 \text{ W} \quad (\text{for a sinusoidal output of max. amplitude})$$

$$= \boxed{40 \text{ W}}$$

ii. Since $V_{O_{\text{peak}}} > \frac{2V_{CC}}{\pi} = \frac{2(62.5)}{\pi} = 40 \text{ V}$, we must find the transistor requirements based on a peak of 40V

$$\text{For } V_{O_{\text{peak}}} = 40 \text{ V}, P_L = \frac{(40 \text{ V})^2}{2(50 \Omega)} = 16 \text{ W}; P_{PS} = 2V_{CC} i_{PS_{\text{ave}}}$$

$$P_{PS} = 2(62.5 \text{ V}) \left(\frac{40 \text{ V} / 50 \Omega}{\pi} \right) = 31.83 \text{ W}$$

$$2P_D = P_{PS} - P_L = 31.83 \text{ W} - 16 \text{ W} = 15.83 \text{ W}$$

$$P_D = 15.83 \text{ W} / 2 = \boxed{7.915 \text{ W} = P_D}$$

$$\boxed{i_{C_{\text{ave}}} = i_{PS_{\text{ave}}} = 0.318 \text{ A}}$$

$$\boxed{i_{C_{\text{max}}} = I_{L_{\text{peak}}} = 1 \text{ A}}$$

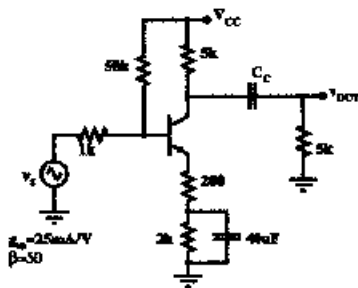
$$\boxed{V_{CE_{\text{max}}} = V_{CC} + V_{O_{\text{peak}}} = 112.5 \text{ V}}$$

(c)

$$\eta_{\text{max class A}} = \frac{25 \text{ W}}{156.25 \text{ W}} \times 100\% = \boxed{16\%}$$

$$\eta_{\text{max class B}} = \frac{25 \text{ W}}{40 \text{ W}} \times 100\% = \boxed{62.5\%}$$

4. For the following circuit,



$$r_{\pi} = \frac{50}{25 \text{ mA/V}} = 2 \text{ k}\Omega$$

assume that $C_{\mu} = 10 \text{ pF}$, $C_{\pi} = 50 \text{ pF}$ and $C_C = 10 \mu\text{F}$. Find

(a) the low-frequency poles and zeros, (15 points)

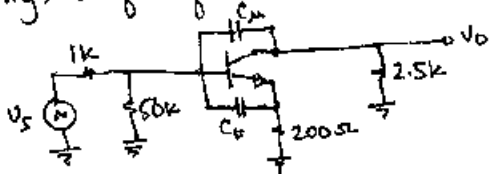
(b) the midband gain. (5 points)

$$(a) \omega_{LC} = \frac{1}{10 \mu\text{F} \times 10 \text{ k}\Omega} = 10 \text{ rps} ; \omega_{LB} = \frac{1}{40 \mu\text{F} \times R_{eqB}}$$

$$R_{eqB} = 2 \text{ k}\Omega \parallel \left[200 + \frac{r_{\pi} + R_B}{\beta + 1} \right] = 2 \text{ k}\Omega \parallel \left[200 + \frac{2 \text{ k}\Omega + 980}{51} \right] = 229 \Omega$$

$$\omega_{L0} = \frac{1}{40 \mu\text{F} \times 229 \Omega} = 109 \text{ rps} ; \omega_{zB} = \frac{1}{40 \mu\text{F} \times 2 \text{ k}\Omega} = 12.5 \text{ rps}$$

(b) high-freq. equivalent circuit:



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